

Topic 1

Hydrodynamics from Boltzmann eqn.

- Hydro
- conservation laws
 - constitutive relations
 - equations of state

Derived balance equations from Boltzmann

continuity equation

$$\frac{\partial}{\partial t} \rho(\mathbf{r}, \vec{v}) + \vec{\nabla}_{\mathbf{r}} \cdot (\rho(\mathbf{r}, \vec{v}) \vec{v}(\mathbf{r}, \vec{v})) = 0$$

momentum balance

$$\frac{\partial}{\partial t} \rho(\mathbf{r}, \vec{v}) \vec{v}(\mathbf{r}, \vec{v}) + \frac{\partial}{\partial \vec{v}_\beta} \left[\rho(\mathbf{r}, \vec{v}) \vec{v}^\beta(\mathbf{r}, \vec{v}) \vec{v}(\mathbf{r}, \vec{v}) + \Pi^{\beta\gamma}(\mathbf{r}, \vec{v}) \right] = \frac{\rho(\mathbf{r}, \vec{v})}{m} \vec{F}^\beta(\mathbf{r}, \vec{v})$$

charge balance

$$\frac{\partial e(\mathbf{r}, \vec{v})}{\partial t} + \vec{\nabla} \cdot \left(\vec{J}_u(\mathbf{r}, \vec{v}) + e(\mathbf{r}, \vec{v}) \vec{v}(\mathbf{r}, \vec{v}) \right) = - \Pi_{\beta\gamma} \frac{\partial v^\beta}{\partial r_\gamma}(\mathbf{r}, \vec{v})$$

along with explicit expressions for

stress tensor $\Pi^{\beta\gamma}(\mathbf{r}, \vec{v}) = \rho(\mathbf{r}, \vec{v}) \left\langle \left(\frac{\vec{p}_\beta}{m} - \vec{v}_\beta(\mathbf{r}, \vec{v}) \right) \left(\frac{\vec{p}_\gamma}{m} - \vec{v}_\gamma(\mathbf{r}, \vec{v}) \right) \right\rangle_{\vec{p}}$

energy flux $\vec{J}_u(\mathbf{r}, \vec{v}) = \frac{1}{2} \rho(\mathbf{r}, \vec{v}) \left\langle \left(\frac{\vec{p}}{m} - \vec{v}(\mathbf{r}, \vec{v}) \right)^2 \left(\frac{\vec{p}}{m} - \vec{v}(\mathbf{r}, \vec{v}) \right) \right\rangle_{\vec{p}}$

where

$$\langle x \rangle_{\vec{p}} = \frac{1}{n(\mathbf{r}, \vec{v})} \int_{\vec{p}} x(\mathbf{r}, \vec{v}, \vec{p}) f(\mathbf{r}, \vec{v}, \vec{p})$$

Now in phenomenological treatment in Chapter I the fluxes Π and \vec{J}_u were fixed by linear constitutive relations, i.e. proportional to gradients

Now this concludes part 1) of the derivation of hydrodynamics, what remains to do soon is how constitutive relations emerge from Boltzmann framework

Generally this will result in reduction of dof's to local thermodynamic properties and/or their gradients

→ Necessary to truncate Boltzmann equation

Note that different truncations are possible corresponding to different expansion schemes / power counting

→ active topic of research in particular for relativistic theories

We will discuss traditional way

based on Chapman-Enskog expansion

which can be viewed as a small expansion in Knudsen number

Chapman Enskog expansion

Since h does not appear explicitly in Boltzmann equation, consider instead $\epsilon \ll 1$

$$\left(\frac{\partial}{\partial t} + \vec{p} \cdot \vec{\nabla}_r + \vec{r} \cdot \vec{\nabla}_p \right) f = \frac{1}{\epsilon} C[f]$$

and expands

$$f(\vec{t}, \vec{r}, \vec{p}) = f^{(0)}(\vec{t}, \vec{r}, \vec{p}) + \epsilon f^{(1)}(\vec{t}, \vec{r}, \vec{p}) + \dots$$

under the assumption that

$$f(\vec{t}, \vec{r}, \vec{p}) = f(T(\vec{t}, \vec{r}), n(\vec{t}, \vec{r}), \vec{v}(\vec{t}, \vec{r}), \vec{p})$$

such that derivatives w.r.t. coordinates can be expressed in terms of derivatives of thermodynamic variables, which are obtained via matching conditions

$$n(\vec{t}, \vec{r}) = \int_{\vec{p}} f(\vec{t}, \vec{r}, \vec{p})$$

$$\vec{v}(\vec{t}, \vec{r}) = \int_{\vec{p}} \frac{\vec{p}}{m} f(\vec{t}, \vec{r}, \vec{p})$$

$$\frac{3}{2} n(\vec{t}, \vec{r}) k_B T(\vec{t}, \vec{r}) = \int_{\vec{p}} \frac{(\vec{p} - m\vec{v}(\vec{t}, \vec{r}))^2}{2m} f(\vec{t}, \vec{r}, \vec{p})$$

Note that expansion may not converge (e.g. asymptotic sources)

Now in order to develop an expansion whose perturbations $f^{(1)}$, $f^{(2)}$, etc in the system are orthogonal to the conserved quantities, we want to absorb the full information about n, \vec{v}, T etc to the leading order distribution,

$$n(\vec{r}, \vec{v}) = \int_{\vec{p}} f(\vec{r}, \vec{p}, \vec{v}) = \int_{\vec{p}} f^{(0)}(\vec{r}, \vec{p}, \vec{v})$$

and similarly for other quantities

Zeroth order: Ideal fluid dynamics

$$O\left(\frac{1}{\epsilon}\right) \quad C[f^{(0)}] = 0$$

$\Rightarrow f^{(0)}$ is local equilibrium solution

$$f^{(0)} = n(\vec{r}, t) \left(\frac{2\pi\hbar^2}{m k_B T(\vec{r}, t)} \right)^{3/2} \exp\left(\frac{-(\vec{p} - m\vec{v}(\vec{r}, t))^2}{2m k_B T(\vec{r}, t)} \right)$$

where $n, v(\vec{r}, t)$ is the same as $n, v(\vec{r}, t)$ in continuity equation, as guaranteed by orthogonality condition

Based on explicit form of $f^{(0)}$ can now calculate $\int_{\mathcal{H}} \Pi^{i5}{}^{(0)}$ at zeroth order

$$\Pi^{i5}{}^{(0)}(\vec{r}, t) = n(\vec{r}, t) \left(\frac{2\pi\hbar^2}{m k_B T(\vec{r}, t)} \right)^{3/2} \int_{\vec{p}} \frac{(\vec{p} - m\vec{v}(\vec{r}, t))^i (\vec{p} - m\vec{v}(\vec{r}, t))^5}{m} \exp(\dots)$$

so perform angular integrals

$$\Pi^{i5}{}^{(0)}(\vec{r}, t) = \frac{2}{3} \theta(\vec{r}, t) \delta^{i5} \frac{5}{2} n(\vec{r}, t) k_B T(\vec{r}, t) \delta^{i5} \left(\frac{5}{2} \right)$$

so

$$\boxed{\Pi^{i5}{}^{(0)}(\vec{r}, t) = P(\vec{r}, t) \delta^{i5}}$$

conversely for

$$\int_{\mathcal{H}} \sum_{\mathcal{H}}^{(0)}(\vec{r}, t) = n(\vec{r}, t) \left(\frac{2\pi\hbar^2}{m k_B T(\vec{r}, t)} \right)^{3/2} \int_{\vec{p}} \frac{(\vec{p} - m\vec{v}(\vec{r}, t))^2}{2m} \left(\frac{\vec{p} - m\vec{v}(\vec{r}, t)}{m} \right) \exp(\dots)$$

vanishes since integrand is odd function of $\vec{p} - m\vec{v}(\vec{r}, t)$

$$\boxed{\int_{\mathcal{H}}^{(0)}(\vec{r}, t) = 0}$$

So using this result we get

$$\rho \left[\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \right] = -\nabla p + \rho \vec{F}$$

$$\frac{\partial \vec{v}}{\partial t} + \nabla (e\vec{v}) = -\rho (\nabla \vec{v})$$

which are EOMs of fluid
dynamics

First order:

$$\mathcal{O}(\epsilon^0) \left(\frac{\partial}{\partial t} + v \vec{\nabla}_r + \vec{\tau} \vec{\nabla}_p \right) \psi^{(0)} = \mathcal{SC}[\psi^{(0)}, \psi^{(1)}]$$

Will perform RTA: $\mathcal{SC}[\psi^{(0)}, \psi^{(1)}] = -\frac{1}{\tau_R} \psi^{(1)}$

and hence

$$\psi^{(1)} = -\tau_R \left(\frac{\partial}{\partial t} + v \vec{\nabla}_r + \vec{\tau} \vec{\nabla}_p \right) \psi^{(0)}$$

Now the challenge to a certain extent is to evaluate the various derivatives, i.e.

$$\frac{\partial}{\partial t} \psi^{(0)} = \frac{\partial n}{\partial t} \frac{\partial \psi^{(0)}}{\partial n} + \frac{\partial T}{\partial t} \frac{\partial \psi^{(0)}}{\partial T} + \frac{\partial \vec{v}}{\partial t} \frac{\partial \psi^{(0)}}{\partial \vec{v}}$$

when to this order in the expansion it is convenient to use local hydrodynamic equations for n, \vec{v}, T to express e.g.

$$\frac{\partial n}{\partial t} = -\vec{\nabla} \cdot (n \vec{v})$$

and similarly for other terms

Derivatives ~~are~~ of $\frac{\partial}{\partial t} v, \frac{\partial}{\partial t} T$ are of higher order and accounted for in higher orders of expansion

Deriving $\vec{u}_p = \frac{\vec{p}}{m} - \vec{v}(t, \vec{r})$ on Γ_{ind}
 (see Chapter 7.5 in Pöthner for details)

$$f^{(1)} = -Z_R f^{(0)} \left[\frac{1}{T} (\vec{u}_p \cdot \vec{\nabla} T) \left(\frac{m}{2k_B T} \vec{u}_p^2 - \frac{5}{2} \right) + \frac{m}{2k_B T} \left(\frac{\partial v_k}{\partial x_l} + \frac{\partial v_l}{\partial x_k} \right) \left(u_p^k u_p^l - \frac{1}{3} \delta^{kl} u_p^2 \right) \right]$$

and we can now proceed to calculate
 first order corrections to energy flux \vec{J}_u
 and stress tensor Π^{ij}

$$\Pi^{ij} = \Pi^{ij(0)} + \Pi^{ij(1)}$$

$$\Pi^{ij(1)} = m \int_{\mathbb{R}^3} u^i u^j f^{(1)}$$

since first term is odd in u

$$\equiv -\frac{m^2 Z_R}{2k_B T} \left(\frac{\partial v_k}{\partial x_l} + \frac{\partial v_l}{\partial x_k} \right) \int_{\mathbb{R}^3} u_i u_j \left(u^k u^l - \frac{1}{3} \delta^{kl} u^2 \right) f^{(0)}$$

20

Decompose integral in basis of symmetric tensors

$$I^{ijkl} = \int_{\mathbb{S}^2} u_i u_j (u^k u^l - \frac{1}{3} \delta^{kl}) \frac{1}{4\pi} = A \delta_{ij} \delta_{kl} + B \frac{(\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk})}{2}$$

$$\delta_{ij} \delta_{kl} I^{ijkl} = 0$$

$$\delta_{kl} (u^k u^l - \frac{1}{3} \delta^{kl}) = 0$$

$$3A + 3B = 0$$

$$A = -\frac{1}{3} B$$

$$\Pi^{ijkl} = \frac{m^2 c^2}{4\pi} \int_{\mathbb{S}^2} \frac{u_i u_j}{r^3} \frac{u^k u^l}{r^3} \frac{1}{4\pi} = \frac{m^2 c^2}{16\pi^2} \int_{\mathbb{S}^2} \frac{u_i u_j u^k u^l}{r^6} \frac{1}{4\pi}$$

$$= \frac{m^2 c^2}{16\pi^2} \int_{\mathbb{S}^2} \frac{u_i u_j u^k u^l}{r^6} \frac{1}{4\pi}$$

$$= \frac{m^2 c^2}{16\pi^2} \int_{\mathbb{S}^2} \frac{u_i u_j u^k u^l}{r^6} \frac{1}{4\pi}$$

$$\begin{aligned} \delta^{ik} \delta^{jl} T^{ijkl} &= 3A + B \left(\frac{9+3}{2} \right) \\ &= -B + 6B = 5B \end{aligned}$$

$$\begin{aligned} B &= \frac{1}{5} \delta^{ik} \delta^{jl} \int_{\vec{p}} u_i u_j \left(u^k u^l - \frac{1}{3} \vec{u}^2 \delta^{kl} \right) f^{(0)} \\ &= \frac{1}{5} \int_{\vec{p}} u^4 \left(1 - \frac{1}{3} \right) f^{(0)} \\ &= \frac{2}{15} \int_{\vec{p}} u^4 f^{(0)} = 2n \frac{(k_B T)^2}{m^2} \\ &= 15 n \frac{(k_B T)^2}{m^2} \end{aligned}$$

So collecting everything we find

$$\begin{aligned} \Pi^{ij} &= - \frac{m^2 c_R}{2k_B T} 2n \frac{(k_B T)^2}{m^2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \\ &= \left(-\frac{1}{3} \delta_{ij} \delta_{kl} + \frac{\delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk}}{2} \right) \\ &= -n k_B T c_R \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \delta_{ij} \frac{\partial v_k}{\partial x_k} \right) \\ \text{So } \left(\Pi^{ij} = -2\eta \sigma^{ij} \right) &= 2 \sigma^{ij} \end{aligned}$$

$$\text{with } \eta = n k_B T c_R$$

Can also compute dissipative correction
to internal energy flux

$$\vec{J}_u = \vec{J}_u^{(0)} + \vec{J}_u^{(1)}$$

we found from linear constitutive relations
and symmetry that

$$\vec{J}_u = -\kappa \vec{\nabla} T$$

now at leading order $\vec{J}_u^{(0)} = 0$

so only correction

$$\vec{J}_u = \int_{\vec{p}} \frac{(m\vec{u}_p)^2}{2m} \vec{u}_p f^{(1)}$$

$$J_u^i = - \int_{\vec{p}} \frac{\tau_R}{T} \frac{(m\vec{u}_p)^2}{2m} u_p^i u_p^j \left(\frac{m}{2k_B T} u_p^2 - \frac{5}{2} \right) f^{(0)} \frac{\partial f}{\partial r_j}$$

so upon performing
angular integrals $\equiv \kappa \delta^{ij}$

$$\kappa = \frac{1}{3} \int_{\vec{p}} \frac{\tau_R}{T} \frac{u_p^2}{2m} u_p^2 \left(\frac{m}{2k_B T} u_p^2 - \frac{5}{2} \right) f^{(0)}$$

$$\equiv \frac{\tau_R}{3Tm^2} \int_{\vec{p}} \frac{(m\vec{u}_p)^2}{2m} (m\vec{u}_p)^2 \left(\frac{(m\vec{u}_p)^2}{2mk_B T} - \frac{5}{2} \right) f^{(0)}$$

$$= \frac{\tau_R}{3Tm^2} e \left(\frac{35}{2} - \frac{25}{2} \right) mk_B T$$

$\underbrace{\hspace{10em}}_{\equiv \frac{3}{2} k_B T = 5}$

$$\boxed{\kappa = \frac{5}{2} \frac{n k_B^2 T \tau_R}{m}}$$

We see that transport coefficients η, κ are proportional to relaxation time τ_R which generally should be a function of $T(t, \vec{r}), n(t, \vec{r})$

→ Smaller relaxation time → smaller avg. distance from local equilibrium

→ Smaller viscosity → more ideal fluid

Can estimate further that

$$\tau_R \sim \tau_{imp} \sim \frac{1}{n \langle v \rangle} \quad \langle v \rangle \sim \sqrt{\frac{k_B T}{m}}$$

$$\Rightarrow \eta = n k_B T \tau_R \sim \frac{\sqrt{m k_B T}}{\sigma_{tot}}$$

approximately independent of density n
and inversely proportional to total cross
section σ_{tot}